

**Subject:** magnetizing inductance...

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So I'm going to do some minor backpedaling regarding the magnetizing inductance thing. I figured I better be able to back up all the smack talk I'm giving you about it, so I started writing the equations for a transformer - actively looking to put them in the form you always draw (with the mag inductance). And as far as I can tell it's even simpler than the whole "reflected impedance" crap I was talking about today (which is a bit more involved and actually has some usefulness). If you write KVL for the primary loop of a transformer (see my ugly drawing attached), you get:

$$V_{in} = R_p i_p + L_p \frac{d(i_p)}{dt} - M \frac{d(i_s)}{dt} \quad \{1\}$$

where  $V_{in}$  is the input voltage (that you apply),  $R_p$  is the primary resistance,  $L_p$  is the primary inductance,  $M$  is the mutual inductance (equal to  $\sqrt{L_p L_s}$ ) and  $i_p$  and  $i_s$  are the primary and secondary currents, respectively. This is really bone-head.

Now I'll just group the two derivative terms and factor out and  $L_p$ :

$$V_{in} = R_p i_p + L_p \left[ \frac{d(i_p)}{dt} - \left( \frac{M}{L_p} \right) \frac{d(i_s)}{dt} \right] \quad \{2\}$$

And use the additive property of the derivative:

$$V_{in} = R_p i_p + L_p \frac{d}{dt} \left[ i_p - \left( \frac{M}{L_p} \right) i_s \right] \quad \{3\}$$

Now let's call the quantity in brackets  $i_m$  (the magnetizing current) and call  $L_p$  the magnetizing inductance ( $L_m$ ). So we can rewrite as:

$$V_{in} = R_p i_p + L_m \frac{d(i_m)}{dt} \quad \{4\}$$

And that's all there is to it. So now you draw the transformer the way you did today (with the mag inductance). And you get to replace the real transformer (that has primary, secondary and mutual inductances) with an ideal (or perfect or whatever you call it) transformer where the voltages and currents are simply related by the turns ratio (which is the same as the sqrt of the inductance ratio). But the current through the mag inductance is a weird combination of the actual primary and secondary currents. And the current into the "ideal" primary is a scaled version of the actual secondary current. I'm at a total loss to see why anyone would want to do the analysis this way. It simplifies the equations a little bit, but at the expense of losing touch with what's really happening. After staring at it for awhile, you can see that the quantity in brackets in {3} (which we're calling the mag current) is a scaled version of the total flux in the transformer core. This explains why the  $i_m$  waveform in your notes looks like it did. Come to think of it, I could have factored out something other than  $L_p$  in eqn {2} such that the quantity left in brackets was exactly equal to the total flux. Then  $L_m$  would have been equal to something other than  $L_p$ . Still I don't get why people bother.

Anyway, I can't believe I just typed so many equations in an email, so I'll stop now. Bottom line is:

- 1) magnetizing inductance is NOT a function of load impedance like I was spewing today (minus 10 points for me); and
- 2) I still think modeling a TXF this way is stupid! Actually I hate it more now than I did earlier today.

-jb

Visio-txf drawing.pdf

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